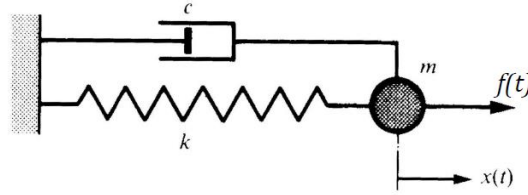


Systèmes avec 1 DDL (degré de liberté)



Equation générale du mouvement (4 formes équivalentes)

$m\ddot{x} + c\dot{x} + kx = f(t)$	$\ddot{x} + \frac{c}{m}\dot{x} + \frac{k}{m}x = \frac{f(t)}{m}$	$\ddot{x} + 2\lambda\dot{x} + \omega_0^2x = \frac{f(t)}{m}$	$\ddot{x} + 2\eta\omega_0\dot{x} + \omega_0^2x = \frac{f(t)}{m}$
$\omega_0 = \sqrt{\frac{k}{m}}$	$\eta = \frac{\lambda}{\omega_0} = \frac{c}{2m\omega_0}$	Libre $\rightarrow f(t) = 0$ Conservatif $\rightarrow c = 0$	Forcé $\rightarrow f(t) \neq 0$ Dissipatif $\rightarrow c \neq 0$

Système libre sur-amorti ($\eta > 1$)

$x(t) = Ae^{-r_1 t} + Be^{-r_2 t}$	$r_1 = \omega_0 (\eta + \sqrt{\eta^2 - 1})$	$r_2 = \omega_0 (\eta - \sqrt{\eta^2 - 1})$
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Système libre sous-amorti ($\eta < 1$)

$x(t) = X_{\text{libre}} e^{-\lambda t} \cos(\omega_1 t - \varphi_{\text{libre}})$	$\omega_1 = \omega_0 \sqrt{1 - \eta^2}$	$x(t_{n+1}) = x(t_n) e^{-\frac{2\pi\lambda}{\omega_1}}$
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Puissance dissipée $\overline{p(t)} = c\overline{\dot{x}^2}$ Pour systèmes libres, X_{libre} et φ_{libre} dépendent sur les conditions initiales

Système forcé – Régime permanente harmonique ($f(t) = F \cos(\omega t)$)

$x(t) = X_{forcé} \cos(\omega t - \varphi_{forcé})$	$X_{forcé} = \frac{F}{\sqrt{(k - m\omega^2)^2 + (c\omega)^2}} \rightarrow X_{forcé} = \frac{\frac{F}{k}}{\sqrt{(1 - \beta^2)^2 + (2\eta\beta)^2}} = X_s \mu(\beta, \eta)$	
	$\tan(\varphi_{forcé}) = \frac{c\omega}{k - m\omega^2} = \frac{2\eta\beta}{1 - \beta^2}$	$\beta = \frac{\omega}{\omega_0}$

$x(t) = \text{Re}(\underline{x}(t))$	$\underline{x}(t) = \frac{\underline{f}(t)}{k - m\omega^2 + jc\omega} = \frac{\underline{f}(t)}{k} \underline{H}(\beta, \eta) = \frac{F}{k} \frac{e^{j(\omega t - \varphi)}}{\sqrt{(1 - \beta^2)^2 + (2\eta\beta)^2}}$	$\underline{H}(\beta, \eta) = \frac{1}{1 - \beta^2 + j2\eta\beta}$
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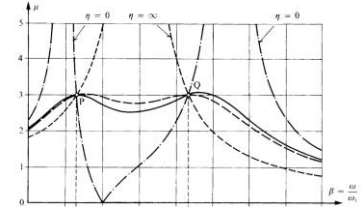
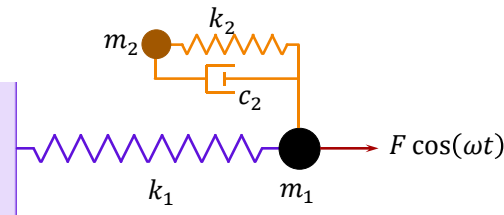
Résonance en amplitude	Résonance en vitesse et phase	Résonance en accélération
$\omega_2 = \omega_0 \sqrt{1 - 2\eta^2}$	ω_0	$\omega_3 = \omega_0 / \sqrt{1 - 2\eta^2}$
$\mu(\beta_2, \eta) = (2\eta)^{-1} (1 - \eta^2)^{-1/2}$	$\mu(\beta_0, \eta) = (2\eta)^{-1}$	$\mu(\beta_3, \eta) = (1 - 2\eta^2)(2\eta)^{-1} (1 - \eta^2)^{-1/2}$

Puissance dissipée : $\overline{p(t)} = c\overline{\dot{x}^2} = \overline{f(t)\dot{x}(t)} = \frac{F^2}{m\omega_0} \frac{\eta\beta^2}{(1 - \beta^2)^2 + (2\eta\beta)^2}$

Système forcé – Régime permanente périodique ($f(t) = f(t + T) = f(t + 2\pi/\omega)$)

$f(t) = \frac{F_0}{2} + \sum_{n=1}^{\infty}(A_n \cos(n\omega t) + B_n \sin(n\omega t))$		$A_n = \frac{2}{T} \int_0^T f(t) \cos(n\omega t) dt$	$B_n = \frac{2}{T} \int_0^T f(t) \sin(n\omega t) dt$
$f(t) = \frac{F_0}{2} + \sum_{n=1}^{\infty} F_n \cos(n\omega t - \psi_n)$		$F_n = \sqrt{A_n^2 + B_n^2}$	$\tan(\psi_n) = B_n/A_n$
$x(t) = \frac{F_0}{2k} + \sum_{n=1}^{\infty} X_n \cos(n\omega t - \psi_n - \varphi_n)$		$\mu_n = \frac{1}{\sqrt{(1 - n^2\beta^2)^2 + (2\eta n\beta)^2}}$	$\tan(\varphi_n) = \frac{2\eta n\beta}{1 - n^2\beta^2}$
$\underline{f}(t) = D_0 + \sum_{n=1}^{\infty} \underline{D}_n e^{jn\omega t}$	$\underline{x}(t) = \frac{D_0}{k} + \sum_{n=1}^{\infty} \frac{\underline{H}_n}{k} \underline{D}_n e^{jn\omega t}$	$\underline{D}_n = \frac{2}{T} \int_0^T f(t) e^{-jn\omega t} dt$	$\underline{H}_n = \frac{1}{1 - n^2\beta^2 + j2\eta n\beta}$

Amortisseur de Frahm



$x_1(t) = Re(\underline{x}_1) \rightarrow \underline{x}_1 = \underline{A}_1 e^{j\omega t} = X_1 e^{-\varphi_1} e^{j\omega t}$	$\underline{A}_1 = F \frac{(k_2 - \omega^2 m_2) + j\omega c_2}{(k_1 - \omega^2 m_1)(k_2 - \omega^2 m_2) - \omega^2 m_2 k_2 + j\omega c_2 (k_1 - \omega^2 (m_1 + m_2))}$			
$\mu_1^2 = \frac{X_1^2}{X_{1s}^2} = \frac{4\eta^2 \beta^2 + (\beta^2 - \alpha^2)^2}{4\eta^2 \beta^2 (\beta^2 (1 + \varepsilon) - 1)^2 + (\varepsilon \alpha^2 \beta^2 - (\beta^2 - 1)(\beta^2 - \alpha^2))^2}$	$\varepsilon = \frac{m_2}{m_1}$	$\alpha = \frac{\omega_2}{\omega_1}$	$\omega_1 = \sqrt{\frac{k_1}{m_1}}$	$\beta = \frac{\omega}{\omega_1}$
$\mu_2^2 = \frac{X_2^2}{X_{1s}^2} = \frac{4\eta^2 \beta^2 + \alpha^4}{4\eta^2 \beta^2 (\beta^2 (1 + \varepsilon) - 1)^2 + (\varepsilon \alpha^2 \beta^2 - (\beta^2 - 1)(\beta^2 - \alpha^2))^2}$	$\eta = \frac{c_2}{2m_2 \omega_1}$		$\omega_2 = \sqrt{\frac{k_2}{m_2}}$	$X_{1s} = \frac{F}{k_1}$
Optimisé pour limiter mouvement de m_1 sur une large plage fréquentielle :				
$\alpha = \frac{1}{1+\varepsilon} = \frac{m_1}{m_1+m_2}$	$\beta_P^2 = \frac{1}{1+\varepsilon} \left(1 - \sqrt{\frac{\varepsilon}{2+\varepsilon}}\right); \beta_Q^2 = \frac{1}{1+\varepsilon} \left(1 + \sqrt{\frac{\varepsilon}{2+\varepsilon}}\right)$		$\mu_{1,P} = \mu_{1,Q} = \sqrt{\frac{2+\varepsilon}{\varepsilon}}$	η pour μ_1 maximum à P ou Q

Systèmes avec n DDL

$\begin{pmatrix} m_{11} & \cdots & m_{1n} \\ \vdots & \ddots & \vdots \\ m_{n1} & \cdots & m_{nn} \end{pmatrix} \begin{pmatrix} \ddot{x}_1 \\ \vdots \\ \ddot{x}_n \end{pmatrix} + \begin{pmatrix} c_{11} & \cdots & c_{1n} \\ \vdots & \ddots & \vdots \\ c_{n1} & \cdots & c_{nn} \end{pmatrix} \begin{pmatrix} \dot{x}_1 \\ \vdots \\ \dot{x}_n \end{pmatrix} + \begin{pmatrix} k_{11} & \cdots & k_{1n} \\ \vdots & \ddots & \vdots \\ k_{n1} & \cdots & k_{nn} \end{pmatrix} \begin{pmatrix} x_1 \\ \vdots \\ x_n \end{pmatrix} = \begin{pmatrix} f_1 \\ \vdots \\ f_n \end{pmatrix}$		$\mathbf{M}\ddot{\vec{x}} + \mathbf{C}\dot{\vec{x}} + \mathbf{K}\vec{x} = \vec{f}$
Systèmes satisfaisant Caughey :	$\mathbf{C} \cdot \mathbf{M}^{-1} \cdot \mathbf{K} = \mathbf{K} \cdot \mathbf{M}^{-1} \cdot \mathbf{C}$	
Matrice noyau : $\mathbf{A} = \mathbf{M}^{-1}\mathbf{K}$	$\det(\mathbf{A} - \delta \mathbb{I}) = 0 \rightarrow \{\delta_1, \cdots, \delta_n\} \text{ valeurs propres} \rightarrow \omega_{0i} = \sqrt{\delta_i} \text{ freqs propres}$	
	$\mathbf{A} \cdot \vec{v}_i = \omega_{0i}^2 \cdot \vec{v}_i \rightarrow \vec{v}_i \text{ vecteurs propres} \rightarrow \mathbf{B} = (\vec{v}_1 \quad \dots \quad \vec{v}_n)$	
Quotient de Rayleigh : $R(\vec{v}) = \frac{\vec{v}^T \mathbf{K} \vec{v}}{\vec{v}^T \mathbf{M} \vec{v}}$	$R(\vec{v}_i) = \frac{\vec{v}_i^T \mathbf{K} \vec{v}_i}{\vec{v}_i^T \mathbf{M} \vec{v}_i} = \frac{k_i}{m_i} = \omega_{0i}^2$	$R(\text{proche de } \vec{v}_i) \approx \omega_{0i}^2$
Relation entre coordonnées modales et réelles : $\vec{x} = \mathbf{B} \cdot \vec{q}$		$\mathbf{M}^0 = \mathbf{B}^T \mathbf{M} \mathbf{B}; \quad \mathbf{C}^0 = \mathbf{B}^T \mathbf{C} \mathbf{B}; \quad \mathbf{K}^0 = \mathbf{B}^T \mathbf{K} \mathbf{B}$
$\mathbf{\Omega}_0^2 = \mathbf{M}^{0^{-1}} \mathbf{K}^0 = \mathbf{B}^{-1} \mathbf{M}^{-1} \mathbf{K} \mathbf{B}$	$2\mathbf{\Lambda} = \mathbf{M}^{0^{-1}} \mathbf{C}^0 = \mathbf{B}^{-1} \mathbf{M}^{-1} \mathbf{C} \mathbf{B}$	$\mathbf{\Omega}_0^2 \text{ et } 2\mathbf{\Lambda} \text{ diagonales avec } \omega_{0i}^2 \text{ et } 2\lambda_i$
Système découplé, résoudre n fois 1 DDL :	$\mathbf{M}^0 \ddot{\vec{q}} + \mathbf{C}^0 \dot{\vec{q}} + \mathbf{K}^0 \vec{q} = \vec{f}^0 = \mathbf{B}^T \vec{f}$	$\ddot{\vec{q}} + 2\mathbf{\Lambda} \dot{\vec{q}} + \mathbf{\Omega}_0^2 \vec{q} = \mathbf{M}^{0^{-1}} \vec{f}^0$
Conservatif :	$\vec{x} = \sum_{i=1}^n \frac{\vec{v}_i}{m_i^0 \omega_{0i}} \left(\int_0^t f_i^0(t - \tau) \sin(\omega_{0i} \tau) \, d\tau + \vec{v}_i^T \mathbf{M} \, \dot{\vec{x}}_{ini} \sin(\omega_{0i} t) + \omega_{0i} \vec{v}_i^T \mathbf{M} \, \vec{x}_{ini} \cos(\omega_{0i} t) \right)$	
Forcé harmonique :	$\underline{\vec{X}}(j\omega) = \sum_{i=1}^n \vec{v}_i \underline{Q}_i(j\omega) = \left[\sum_{i=1}^n \frac{\vec{v}_i \otimes \vec{v}_i}{m_{0i}(-\omega^2 + 2j\eta_i \omega_{0i} \omega + \omega_{0i}^2)} \right] \underline{\vec{F}}(j\omega) = \underline{H}(j\omega) \underline{\vec{F}}(j\omega)$	

Systèmes Continus

Vibration (y) de Cordes : (σ contrainte, ρ densité)	$\frac{\partial^2 y}{\partial t^2} = a^2 \frac{\partial^2 u}{\partial x^2} = \frac{\sigma}{\rho} \frac{\partial^2 y}{\partial x^2}$	Vibration (u) de Barres : (E module de Young, ρ densité)	$\frac{\partial^2 u}{\partial t^2} = a^2 \frac{\partial^2 u}{\partial x^2} = \frac{E}{\rho} \frac{\partial^2 u}{\partial x^2}$
Vibration (φ) en Torsion : (G module de glissement, ρ densité)	$\frac{\partial^2 \varphi}{\partial t^2} = a^2 \frac{\partial^2 \varphi}{\partial x^2} = \frac{G}{\rho} \frac{\partial^2 \varphi}{\partial x^2}$	Solution : $\left(A_n \cos\left(\frac{\omega_n}{a} x\right) + B_n \sin\left(\frac{\omega_n}{a} x\right) \right) \cos(\omega_n t)$	
Vibration (y) de poutres droites : (I moment d'inertie, A aire de la section)	$\frac{\partial^2 y}{\partial t^2} = -\frac{EI}{\rho A} \frac{\partial^4 y}{\partial x^4}$		
Solution :	$y_n(x, t) = \left(A_n \cos\left(\frac{\alpha_n}{L} x\right) + B_n \sin\left(\frac{\alpha_n}{L} x\right) + C_n \cosh\left(\frac{\alpha_n}{L} x\right) + D_n \sinh\left(\frac{\alpha_n}{L} x\right) \right) \cos(\omega_n t)$		$\left(\frac{\alpha_n}{L}\right)^4 \frac{EI}{\rho A} = \omega_n^2$